



INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁶ :

F23G 5/24

A1

(11) International Publication Number:

WO 98/10224

(43) International Publication Date:

12 March 1998 (12.03.98)

(21) International Application Number: PCT/FI96/00466

(22) International Filing Date: 2 September 1996 (02.09.96)

(71) Applicant (for all designated States except US): FIOTER OY
(FI/FI); Lastaajanväylä 22, FIN-53420 Lappeenranta (FI).

(72) Inventors; and

(75) Inventors/Applicants (for US only): MANELIS, Georgi
[RU/RU]; (RU). FOURSOV, Viktor [RU/RU]; (RU).
STESIK, Lev [RU/RU]; (RU). YAKOVLEVA, Galina
[RU/RU]; (RU). GLAZOV, Sergei [RU/RU]; (RU).
POLIANTCHIK, Evgueni [RU/RU]; (RU). ALKOV,
Nikolai [RU/RU]; Academy of Sciences, Institute of
Chemical Physics in Chernogolovka, Chernogolovka,
Moscow Region, 142432 (RU).(74) Agent: PAPULA REIN LAHTELA OY; Fredrikinkatu 61 A,
P.O. Box 981, FIN-00101 Helsinki (FI).(81) Designated States: AL, AM, AT, AU, AZ, BB, BG, BR, BY,
CA, CH, CN, CZ, DE, DK, EE, ES, FI, GB, GE, HU, IL,
IS, JP, KE, KG, KP, KR, KZ, LK, LR, LS, LT, LU, LV,
MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU,
SD, SE, SG, SI, SK, TJ, TM, TR, TT, UA, UG, US, UZ,
VN, ARIPO patent (KE, LS, MW, SD, SZ, UG), Eurasian
patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European
patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT,
LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI,
CM, GA, GN, ML, MR, NE, SN, TD, TG).

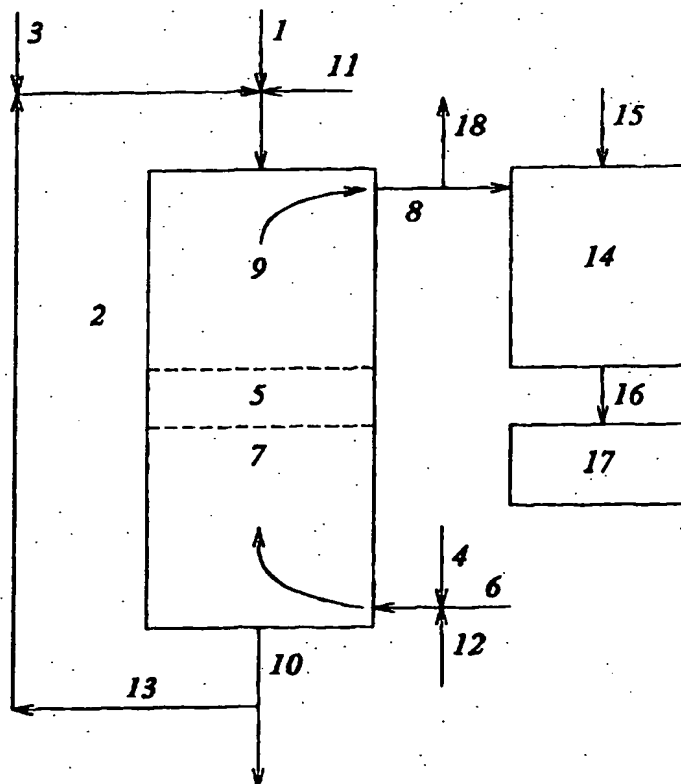
Published

With international search report.

(54) Title: METHOD FOR TREATING WASTE MATERIAL CONTAINING HYDROCARBONS

(57) Abstract

The present invention relates to a method for treating waste material containing hydrocarbon, wherein the waste material is supplied in a reactor, gas containing oxygen is supplied in the reactor, said substances are combusted to form gaseous combustion products and solid residue and said solid residue is discharged from the reactor. The gas containing oxygen is supplied continuously in the reactor in amounts insufficient for complete oxidation of the waste material, said gas containing oxygen is supplied so as to pass it through a layer of said solid residue and the gaseous combustion products are passed through a layer of untreated waste material to form a product gas containing hydrocarbons and droplets of liquid hydrocarbons.



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece	ML	Mali	TR	Turkey
BG	Bulgaria	HU	Hungary	MN	Mongolia	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MR	Mauritania	UA	Ukraine
BR	Brazil	IL	Israel	MW	Malawi	UG	Uganda
BY	Belarus	IS	Iceland	MX	Mexico	US	United States of America
CA	Canada	IT	Italy	NE	Niger	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NL	Netherlands	VN	Viet Nam
CG	Congo	KE	Kenya	NO	Norway	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NZ	New Zealand	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	PL	Poland		
CM	Cameroon	KR	Republic of Korea	PT	Portugal		
CN	China	KZ	Kazakhstan	RO	Romania		
CU	Cuba	LC	Saint Lucia	RU	Russian Federation		
CZ	Czech Republic	LI	Liechtenstein	SD	Sudan		
DE	Germany	LK	Sri Lanka	SE	Sweden		
DK	Denmark	LR	Liberia	SG	Singapore		
EE	Estonia						

METHOD FOR TREATING WASTE MATERIAL CONTAINING HYDROCARBONS

The present invention relates to a method for treating waste material containing hydrocarbons, wherein said material is supplied to a reactor, gas containing oxygen is supplied to the reactor, said substances are combusted to form solid residue and said solid residue is discharged from the reactor.

In this disclosure waste material containing hydrocarbons means any kind of material containing hydrocarbons (with longer or shorter carbon chain), found in the nature, produced chemically, formed in mineral or mechanical processes, formed through leakings of materials containing hydrocarbon into soil, etc. Especially, the method is directed to treating waste materials, ie. sludges containing heavy liquid and/or solid hydrocarbons, solid incombustible materials, water, etc. Further, the invention provides a method for treating industrial waste materials obtained in thermal treatment of metals and comprising oils, possibly partially oxidized or carbonized, ferrous oxides, and other admixtures; crude oil spills, mixed with solid impurities; slurries and sludges, such as sediments of oil tanks, bituminous sands, etc. Hereafter all such materials are referred to as waste materials.

Waste materials are difficult to process for disposal purposes. The disposal of waste materials through environmentally acceptable incineration, recovering the energy content and recovering their hydrocarbon contents in a processible form by conventional techniques is problematic. Direct incineration of waste materials is usually hampered by their high viscosity and the presence of solids therein, which prevent the application of conventional incineration methods, such as atomization in fuel jets. Isolation

of hydrocarbons by distillation is generally energy consuming.

From patent specification JP 51-33486 a method is known for disposal of oxides containing oil by adding them to an agglomeration mixture with further thermal treatment in a rotary kiln. The hydrocarbons are burnt in the process, yielding additional heat, and the iron oxides enter the mixture. This method has relatively narrow applicability, only in some metallurgical processes, and relatively high energy costs if it is used in oil incineration.

From patent specification RU 1090972 a method is known for disposal of wastes containing oil and iron. In this method, liquid waste oils are dehydrated until the fuel contents of 30 - 95 % is attained and are further burnt at a relatively substoichiometric air (0.35 - 0.65 of stoichiometric oxygen). At the smoke temperature of 950 - 1100 °C, the dehydrated waste is treated with the gaseous combustion products and, after reduction of metal oxides, the gaseous products are afterburnt, the heat of smoke gases being used for dehydration of the waste. The main disadvantage of this method is the stage of water evaporation, which hampers environmental safety of the process and makes the method complicated. Further, the method has a narrow field of economical application.

From the patent specification US 4957048 a method is known, wherein crude oil slurries and other slurries containing heavy hydrocarbons are incinerated. The slurries are mixed with diatomite or perlite so as to obtain a friable mass that is further applied to an incinerator type of rotary kiln or a fluidized bed tubular furnace where the mixture is burnt to yield smoke gases and solid residue that is virtually free of hydrocarbons. The solid residue can be recycled for mixing with fresh oil slurries. This method has a number of disadvantages. The use of conventional

rotary kilns is associated with high energy expenditure. Apart from that, due to the entrainment of particulates in flue gas flow, the system requires a complicated secondary cleansing for smoke gases involving cyclones and/or scrubbers. Another disadvantage of the rotary kiln embodiment is caused by the unburnt carbon present in solid residues. The latter must be afterburnt in a fluidized bed furnace. When fluidized bed reactors are used, the method is sensitive to the size of particulates, both initially contained in waste oil and added in preparing the mixture.

An object of the present invention is to eliminate the drawbacks of the prior art.

Another object of the present invention is to provide an environmentally safe and energy-efficient method for treating a variety of waste materials containing hydrocarbons.

Another object of the present invention is to provide a method for treating waste material containing hydrocarbons, wherein at least a part of the hydrocarbons may be recovered.

Regarding the features characterizing the invention, reference is made to the claims section.

According to the invention gas or gasifying agent containing oxygen is supplied continuously in the reactor in amounts sufficient for complete oxidation of the waste material, said gas or gasifying agent containing oxygen is supplied so as to pass it through a layer of said solid residue and the gaseous combustion products are passed through a layer of untreated waste material to form a product gas containing hydrocarbons and droplets of liquid hydrocarbons. - Accordingly the product gas comprises gaseous combustion products of hydrocarbons. Because of the sub-stoichiometric amount of oxygen, the combustion products comprise carbon monoxide and hydrogen in addition to carbon dioxide and water.

According to an advantageous embodiment, the gas containing oxygen is supplied to the reactor countercurrently to the supply of the waste material so that the combustion zone is formed.

5 Accordingly, the combustion zone is formed in the middle part of the reactor, that means between the ends of the reactor. The gas or gasifying agent containing oxygen is supplied to the reactor at a point after the combustion zone in the streaming direction
10 and the gaseous products are discharged from a point before the combustion zone in the streaming direction of the waste material.

To enhance the yield of hydrocarbons, in order to promote their evaporation, one can introduce
15 steam into the zone where hydrocarbons are heated by the hot product gas.

In the following, the invention is disclosed with nonrestricting examples referring to figs 1 and 2 showing schematical flow charts of two embodiment ex-
20 amples, and with Examples 1 and 2.

For implementing the treating process the waste material charged into the reactor 2 is preferably sufficiently gas-permeable. If the waste material 1 contains enough solid particles of sufficiently
25 large dimension, the waste material 1 can be treated as it is. When the contents of solids of the waste material is low or particle size is too small (so as to hamper gas permeability), the waste material may preferably be, prior to charging into the reactor, be
30 mixed with solid incombustible material 3 that has a melting point high enough to avoid agglomeration; the solid material may be e.g. firebrick pieces. Alternatively, the solid inert material may be charged into the reactor without preliminary mixing it with the
35 waste material (e.g., in intermittent layers) if this mode of charging secures sufficient gas permeability and homogeneity on the average of the charge. To se-

cure high gas permeability, the inert material having predominantly pieces size over 20 mm may be used. The experiments carried out have shown that with this size of particles the pressure drop in the charge at the gas flow rate of 1000 m³/h of per 1 m² reactor cross-section did not exceed 500 Pa/m. This makes it possible to perform a process at low pressure drop in the reactor, this drop may be provided with a fan and not a compressor. As this inert material pieces of waste refractory or some special items such as tubular cylinders may be used.

The process may be initiated by injecting into the reactor gas or gasifying agent containing oxygen, preliminary heated to a temperature over 400 °C. The preheated gasifying agent may be supplied during a time sufficient to establish in the reactor the zone of gasification. This zone establishes as a result of ignition of the changed waste material in a section of the reactor adjacent the gasifying agent inlet. As a result, a processing zone establishes in the reactor. In this zone, as the charge heats up, the following processes occur successively. Light hydrocarbons condense forming suspended fine droplets of oil, lighter fractions of the waste oil material evaporate, heavier fractions of waste oil material pyrolyze yielding char, the char and possibly a part of heavy organics burn.

The combustion zone moves with respect to the charge. When a stationary processing zone establishes in the reactor, the preheating of the gasifying agent is redundant and cool gasifying agent is supplied to the reactor substoichiometrically, in the amount insufficient for complete oxidation of organics; the gasifying agent being supplied so as to pass it through a layer of hot solid residue free of carbon and hydrocarbons formed as the processing zone propagates over the charge. The product gas formed in

the processing zone 5, which bears fine droplets of condensed hydrocarbons (and possibly water) generally contains carbon mono- and dioxide, nitrogen, hydrogen, hydrocarbon gases, etc. The product gas is directed through a layer 9 of an unprocessed waste material and withdrawn or discharged from the reactor.

The process described can be performed either in a continuous mode or in batches. In the first case the waste material (processing mixture) is supplied to the reactor continuously or in portions and the solid residue of the process is discharged from the reactor continuously or in portions. In the second case, the reactor is recharged after the charge was processed and the reactor extinguished. In the first case, the processing zone remains on average stationary with respect to the reactor, although it propagates with respect to countercurrently moving charge. In the second case, the processing zone moves along the stationary charge with respect to the reactor.

The processing in the system when the gasifying agent 6 and then the product gas 8 successively passes through the solid residue of the process 10 and the solid charge, respectively, owing to interface heat exchange, provides a possibility to substantially reduce both temperature of the product gas and that of the solid residue. This provides a possibility to accumulate heat in the zone where the combustion occurs and secures complete burning of the char. Apart from that, unlike in the prior art, the filtration of the product gas through fresh oil allows to prevent entrainment of particulates in the gas flow; this dramatically simplifies further cleansing of smoke gases. Another advantage over the prior is that this method, once initiated, is self-sustained with the heat of the combustion and does not require any additional energy supply. However, when waste material or oils containing extremely little of non-volatile organic matter is

to be processed, one may use the present method by intentionally adding some solid fuel 11 (e.g. up to 10 % by weight) to the charge. Such a solid fuel can be any one of organic containing carbon, in particular, wood, textile, pulp waste, peat or coal fines, etc.

The present method, since it is distinguished by the accumulation of the combustion heat in the processing zone (the heat is stored by the heated solid residue) is stable with respect to fluctuations in flow rates, inhomogeneities of the charge and variations of composition of the gasifying agent. Even after a complete shutoff of supply of the gasifying agent, the process may be relit by simple resumption the supply during the time when the temperature of the charge remains high.

By varying the ratio of the mass of the components of the charge that burn in the combustion zone (contained in the oil and intentionally introduced) to the mass of solid residue, one can widely control the temperature of the combustion zone and the width of the latter. Possible variations are high indeed. Thus experiments on a model composition comprising lubricating oil, coal dust, and pieces of firebrick (26 : 3 : 71 by weight) with air used as a gasifying agent, showed that gasification and afterburning of the product gas proceed steadily without any external heat source; the maximum combustion temperature amounted to 1100 °C. Only at the contents of carbonized fuel lower than 0.02 of the solid residue, the process grows unstable. In the latter case, temperature in the processing zone decreases after ignition and the process extinguishes. An increase in the above ratio until a certain ratio that depends on the particular composition of waste oil results in higher temperature in the combustion zone and enhanced width of the latter. Over this limit the combustion temperature decreases in spite of higher concentration of the solid fuel. This

reduction is due to lower accumulation of heat by the solids in the processing zone.

When processing waste oils with a high content of heavy fractions (high yield of char) one can, in order to reduce the maximum temperature of combustion and improve the calorific value of the product gas, introduce water in the gasifying agent so as to relay heat effect of combustion to the product gas owing to water gas reactions.

The solid residues of the process that pass through the combustion zone are substantially free of hydrocarbons, char, and organics. In most cases, they can be easily disposed of. In particular, the processing of waste oils of metallurgy may yield useful products, such as ferrous oxides that might be used. The solid residue or its part, possibly after elimination of fines, may be reused for making the mixture to be charged into the reactor.

The product gas may be easily and environmentally friendly disposed of using known techniques. In particular, it may be burnt in an afterburner, whereinto secondary air sufficient for complete oxidation of hydrocarbons is injected. Small size of the hydrocarbon droplets secures fast, complete, and clean combustion thereof. The heat released in aftercombustion may be used, e.g. by directing smoke gases to boiler.

In some cases it is economical to direct, prior to afterburning, the product gas into a condenser, wherein at least a part of the condensable hydrocarbons, which are substantially free of solids and are typically composed of lighter fractions than the initial oil, may be recovered and directed for use according to conventional techniques.

Figure 2 schematically presents an embodiment example of the method in the case when the hydrocarbons produced have no other value but for their heat

contents. In this example a secondary combustion is performed in the reactor 2, in a part of its volume 19 that is substantially free of processing mixture and wherein the secondary air 15 for complete burning of the product gas is injected.

EXAMPLE

In laboratory experiments the materials presented in the table 1 were mixed with firebrick pieces size of 20 to 50 mm (1-3, 5 or 7-10 mm (4, 6) and solid fuel in quantities shown in the table.

TABLE 1

Mater	HC, %/w	ASH, %/w	HUM, %/w	ADF, %/w	I , %/w	STM, %/w	HCR, %/w	PR, m/h
1 IND	80	10	10	-	79	2*	...*	1.7
2 IND	80	10	10	-	79	30	50	1.9
3 LBR	95	2	3	10**	65	0	70	1.6
4 SED	60	30	10	8***	67	20	63	2.3
5 SOIL	18	36	46	8**	67	2*	...*	2.1
6 PTS	16	80	4	7**	40	20	47	1.5
7 ASP	19	79	2	-	-	20	...*	1.2

- 15 * natural air humidity
- * product gas was afterburnt directly
- ** coal fines
- *** sawdust

20 In the table 1, IND is spent industrial oil of thermal treatment, LBR is spent lubricant oil, SED is sediment from a black oil tank, SOIL is soil contaminated with crude oil and lubricant oils spill, BTS is bituminous sand and ASP is asphalt.

25 HC is hydrocarbons content in material, ASH is ash content, HUM is humidity; ADF is the quantity of solid fuel added to the processing mixture, I is the fraction of solid inert material added to the mixture, STM is the fraction of steam in gasifying agent;
30 HCR is the fraction of hydrocarbons recovered in the

form of liquid oil, and PR is linear processing rate of the fresh processing mixture in the reactor (i.e., the linear rate of propagation of the gasification zone along the processing mixture).

5 The prepared mixtures were charged into a cylindrical reactor. The ignition was achieved by means of injecting into the reactor hot (400-450 °C) air for several minutes. In the course of the established process, air at room temperature or 100 °C air-steam
10 mixture was supplied to the reactor. After the process was initiated, the process proceeded with intense formation of the product gas bearing extremely fine (about 1 µm) oil droplets and containing nitrogen, carbon di- and monoxide, hydrogen, and uncondensable
15 hydrocarbons. In certain cases, a fraction of liquid hydrocarbons was condensed in a winding tube to yield liquid oil (collected together with water, with which the oil readily stratified). In all the cases mentioned, the temperature in the processing zone exceeded 800 °C (the maximum value was 1250 °C). The
20 product gas burned steadily with the supply of secondary air in the afterburner. The smoke gases did not contain (within 100 ppm) nitrogen oxides and carbon monoxide. Neither soot nor dust particles were detected in the smoke gases. The solid residue discharged from the reactor was free of char and hydrocarbons. After fractionating it, the firebrick pieces recovered were repeatedly employed for preparation of
25 the mixture.

PATENT CLAIMS

1. A method for treating waste material containing hydrocarbon, wherein the waste material is supplied in a reactor, gas containing oxygen is supplied in the reactor, said substances are combusted to form gaseous combustion products and solid residue and said solid residue is discharged from the reactor, characterized in that gas containing oxygen is supplied continuously in the reactor in amounts insufficient for complete oxidation of the waste material, said gas containing oxygen is supplied so as to pass it through a layer of said solid residue and the gaseous combustion products are passed through a layer of untreated waste material to form a product gas containing hydrocarbons and droplets of liquid hydrocarbons.

2. A method according to claim 1, characterized in that the gas containing oxygen is supplied in the reactor countercurrently to the supply of the waste material through the reactor so that a combustion zone is formed.

3. A method according to claim 1 or 2, characterized in that the waste material is supplied to a vertical reactor type of a shaft kiln and the gas flow in the reactor is directed along the vertical axis of the reactor.

4. A method according to anyone of claims 1 - 3, characterized in that the waste material is supplied to the reactor with inert solid incombustible material.

5. A method according to claim 4, characterized in that the inert solid incombustible material comprises pieces predominantly having mesh size over 20 mm.

6. A method according to claim 4 or 5, characterized in that the waste material

and the inert material are mixed prior to supplying to the reactor.

7. A method according to anyone of claims 4 - 6, characterized in that the solid incombustible material comprises pieces of refractory materials or waste refractory material.

8. A method according to anyone of claims 4 - 7, characterized in that the solid incombustible material is at least partly the solid residue obtained in the process.

9. A method according to anyone of claims 1 - 8, characterized in that solid fuel is supplied to the reactor wherein the amount of the solid fuel is 0 - 10 % by weight of the materials supplied to the reactor.

10. A method according to anyone of claims 1 - 9, characterized in that the maximum temperature in the combustion zone and the width of the combustion zone are controlled by varying the mass ratio of the combustible materials burning within said zone to the solid residue of processing, and that said ratio is maintained over 0.02.

11. A method according to anyone of claims 1 - 11, characterized in that the waste material is supplied to the reactor and the solid residues are discharged from the reactor in batches after processing the charge is completed.

12. A method according to anyone of claims 1 - 10, characterized in that the waste material is supplied to the reactor and the solid residue is discharged from the reactor continuously or in portions without interrupting the process.

13. A method according to anyone of claims 1 - 12, characterized in that water is supplied to the reactor.

14. A method according to claim 13, characterized in that water is supplied

to the reactor down the gas flow with respect to the combustion zone

15. A method according to claim 13 or 14, characterized in that steam is supplied to the reactor together with the gas containing oxygen.

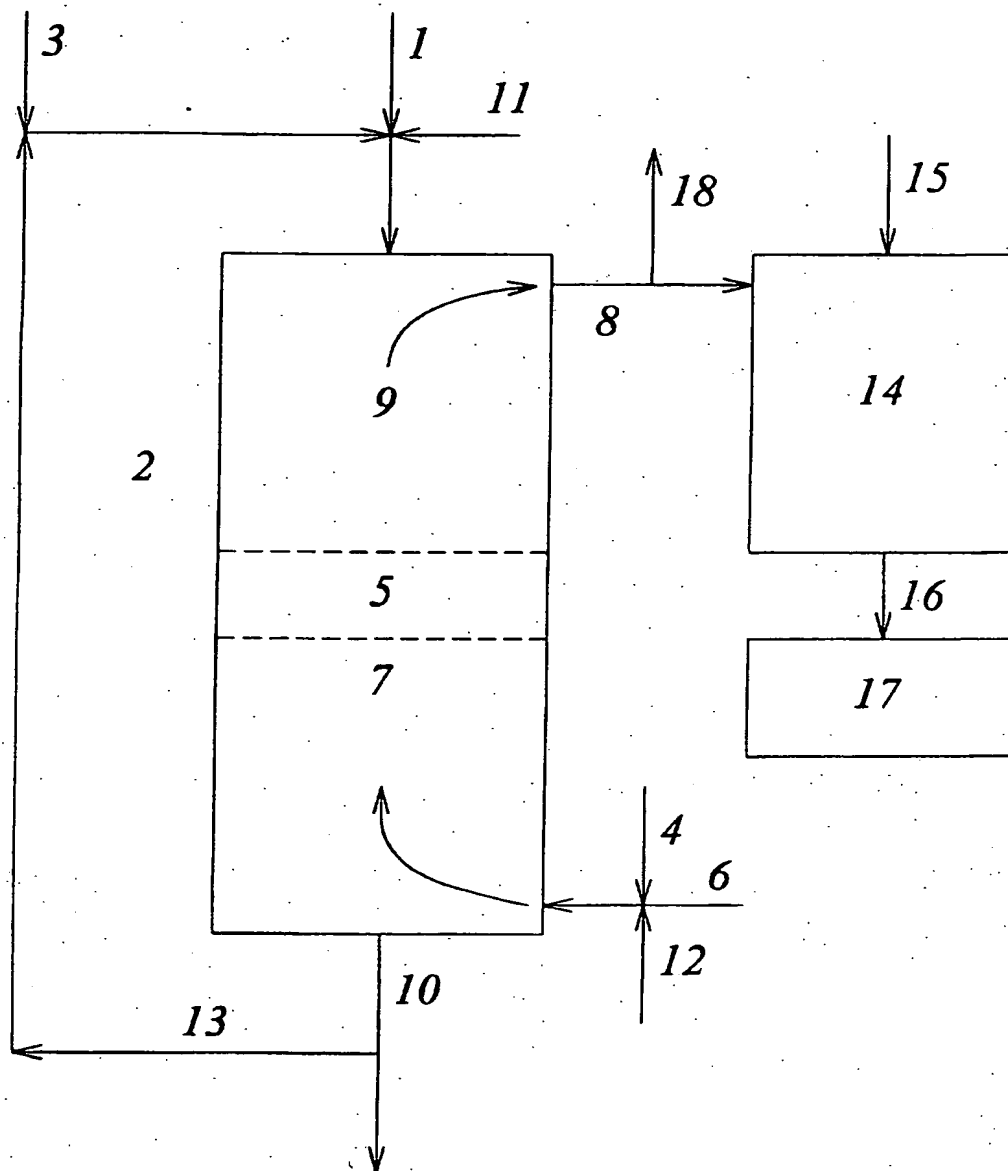
16. A method according to anyone of claims 1 - 15, characterized in that condensable hydrocarbons are recovered from the product gas.

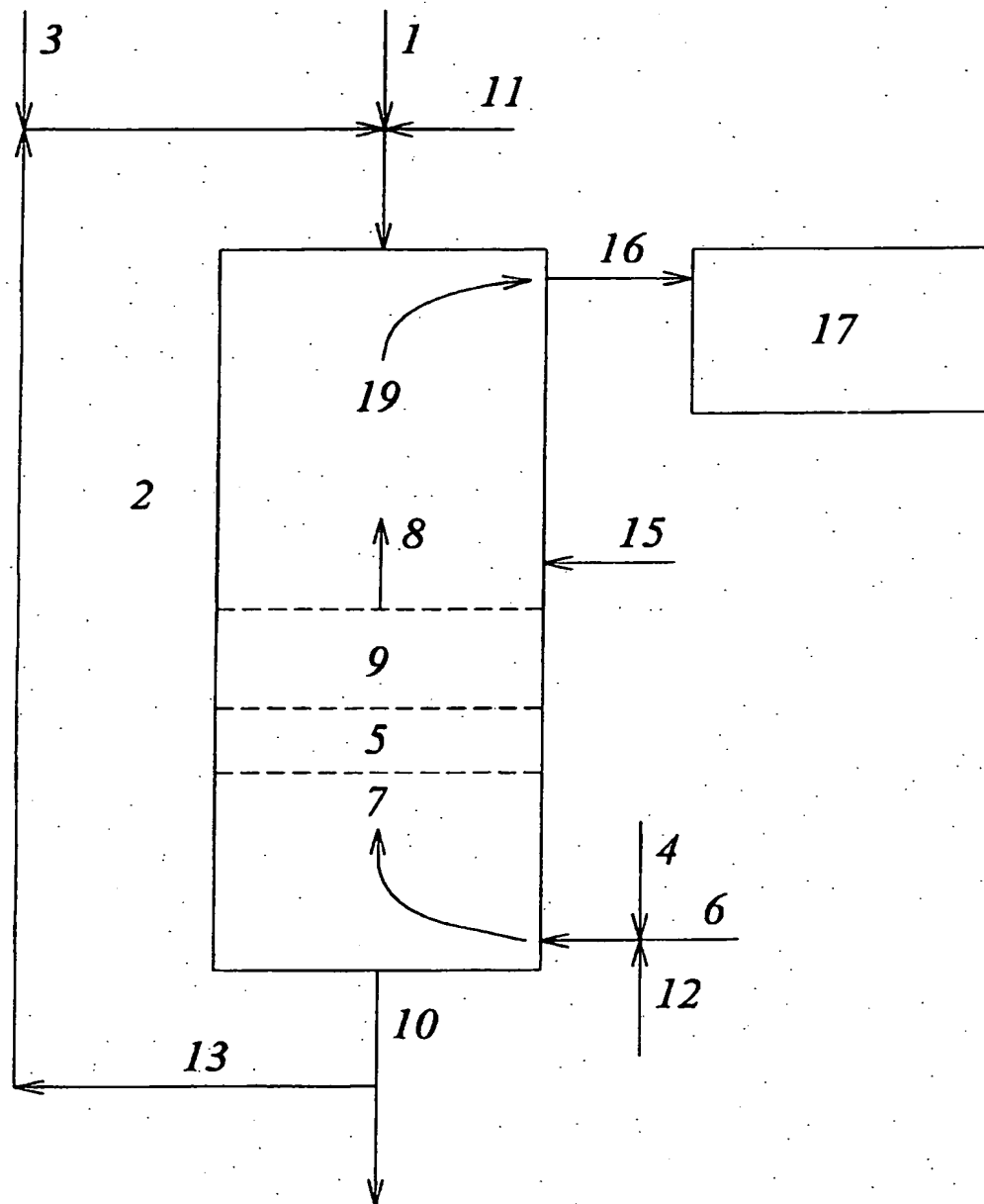
17. A method according to anyone of claims 1 - 16, characterized in that the product gas is afterburnt until complete oxidation of hydrocarbons and combustible gases.

18. A method according to claim 17, characterized in that afterburning is arranged in a part of the reactor, which part is substantially free of the waste material, by supplying hereto air for complete oxidation of hydrocarbons and combustible gases.

19. A method according to claim 17 or 18, characterized in that the heat produced in the afterburning is used in a boiler.

20. A method according to anyone of claims 1 - 19, characterized in that the combustion of the waste material is ignited by injecting air preheated over 400 °C into the reactor.

*Fig. 1*

*Fig. 2*

INTERNATIONAL SEARCH REPORT

International application No.

PCT/FI 96/00466

A. CLASSIFICATION OF SUBJECT MATTER

IPC6: F23G 5/24

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC6: F23G, F23B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

WPI,PAJ,EPODOC

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	SE 389903 B (UNION CARBIDE CORPORATION), 22 November 1976 (22.11.76), page 9 - page 11, figure 1	1-3,16-18
Y	US 5257587 A (OHLSEN ET AL), 2 November 1993 (02.11.93), column 3, line 22 - line 24, figure 1	1-3,16-18
A	US 4957048 A (BEER ET AL), 18 Sept 1990 (18.09.90), column 2, line 43 - column 4, line 27	4-9,11,12
A	US 4931161 A (SUNDAR), 5 June 1990 (05.06.90), column 3, line 50 - column 5, line 60	4,6-7,13

☒ Further documents are listed in the continuation of Box C. ☒ See patent family annex.

* Special categories of cited documents:

"A" document defining the general state of the art which is not considered to be of particular relevance

"B" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

26 May 1997

Date of mailing of the international search report

28-05-1997

Name and mailing address of the ISA/
Swedish Patent Office
Box 5055, S-102 42 STOCKHOLM
Facsimile No. +46 8 666 02 86

Authorized officer

Eva Danielsson
Telephone No. +46 8 782 25 00

Form PCT/ISA/210 (second sheet) (July 1992)

INTERNATIONAL SEARCH REPORT

International application No.

PCT/FI 96/00466

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 3894497 A (HELKE ET AL), 15 July 1975 (15.07.75), column 1, line 44 - line 63 --	17-20
A	US 4967673 A (GUNN), 6 November 1990 (06.11.90), figures 1,2 -----	1-20

Form PCT/ISA/210 (continuation of second sheet) (July 1992)

INTERNATIONAL SEARCH REPORT
Information on patent family members

20/05/97

International application No.

PCT/FI 96/00466

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
SE 389903 B	22/11/76	AR 207097 A AT 317402 B AU 469912 B AU 4433072 A BE 786025 A BR 7204488 D CA 960088 A CH 562427 A DE 2233498 A,C FR 2145529 A GB 1384925 A HK 41077 A NL 172005 B,C NL 7209498 A SE 7508634 A US 3729298 A ZA 7203689 A	15/09/76 26/08/74 26/02/76 21/02/74 08/01/73 00/00/00 31/12/74 30/05/75 25/01/73 23/02/73 26/02/75 12/08/77 17/01/83 11/01/73 30/07/75 24/04/73 28/03/73
US 5257587 A	02/11/93	NONE	
US 4957048 A	18/09/90	CA 1305440 A EP 0303340 A US 4775457 A	21/07/92 15/02/89 04/10/88
US 4931161 A	05/06/90	AU 5819490 A CA 2072376 A WO 9100900 A	06/02/91 13/01/91 24/01/91
US 3894497 A	15/07/75	AU 477104 B AU 6687474 A DE 2412927 A,C FR 2222610 A,B GB 1457948 A JP 898756 C JP 50008381 A JP 52027465 B SE 385730 B,C	14/10/76 16/10/75 26/09/74 18/10/74 08/12/76 25/02/78 28/01/75 20/07/77 19/07/76
US 4967673 A	06/11/90	AU 625936 B AU 4840090 A EP 0448639 A WO 9007085 A	16/07/92 10/07/90 02/10/91 28/06/90

Form PCT/ISA/210 (patent family annex) (July 1992)